ANITIA, N.; ILLE,C.; VOICULESCU, Maria

Potassium influence on sugar beets with different doses of nitrogen. Studii cerc biol veget 15 no.4:479-497 '63.

1. Comunicare prezentata de academician N.Salageanu.

ANITIA, N.; ILLE, C.; VOICULESCU, Maria

Influence of phosphorus and nitrogen on sugar beets. Studii
cerc biol s bot 16 no.6:547-556 '64.

1. Food Research Institute, Bucharest.

sov/129-59-2-4/16

AUTHOR: Anitov, I.S., Candidate of Technical Sciences

TITLE: Carbide Formation During Isothermal Decomposition of

Alloyed Austenite in Hypereutectoidal Steels (Karbidoobrazovaniye pri izotermicheskom raspade legirovannogo austenita zaevtektoidnykh staley)

PERIODICAL: Metallovedeniye i Termicheskaya Obrabotka Metallov,

1959, Nr 2, pp 19 - 22 (USSR)

ABSTRACT: The aim of the here described work was to study the

isolation of the carbide phase during decomposition of the austenite in mono-alloyed steels containing about 0.% C. The investigations were carried out in six hypereutectoidal alloyed steels for which the contents of the carbon, the alloying elements the content of the alloying element in the carbide phase of annealed

steel and the Curie-point temperature of carbides in the annealed steel are entered in Table 1 (this enumeration

follows the sequence of the columns in the table).

The choice of the composition of the steel was governed by the possibility of transforming into solid solution during austenisation a maximum quantity of each alloying element and by obtaining a duration of the decomposition

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SOV/129-59-2-4/16

Carbide Formation During Isothermal Decomposition of Alleyed Austenite in Hypereutectoidal Steels

of over-saturated austenite which is convenient for carrying out the experiments. All the steels were produced in a 5-kg induction furnace; after homogenisation annealing, the rods were forged into 15 x 15 mm sections and then they were annealed at 850 °C. From the rods 3 mm long, 1 mm dia cylindrical specimens were produced for studying the kinetics of decomposition of the austenite and also plates of 60 x 15 x 3 mm for carbide analysis. The kinetics of transformation of the austenite were investigated by means of an instrument of the type of magnetic scales; the process of carbide formation was studied on the basis of the chemical composition and the temperatures of the Curie point of carbide pewders, which were produced by electrolytic solution of specimens after specified regimes of isothermal treatment. The obtained kinetic curves of decomposition of the austenite and of rejection of the alloying elements into the carbide phase are graphed for nickal steel (Figure 2), manganese steel (Figure 2), chromium steel (Figure 2), tungsten

SOV/129-59-2-4/16 Carbide Formation During Isothermal Decomposition of Alloyed Austenite in Hypereutectoidal Steels

vanadium steel (Figure e). It was established that the transition of carbide-forming elements from the solid solution into the carbide phase during isothermal decomposition of super-cooled austenite in hypereutectoidal steels usually occurs prior to and during the main transformation. Manganese and vanadium steels form an exception; in the case of these steels, the transition at 50 °C is completed prior to the main transformation. Excess carbide may exist in the form of alloy cementite; as the process develops, the quantity of allow elements in the cementite increases (the Curie point is lower) and a special carbide is formed. It can be assumed that in a number of cases, it would not be possible to detect experimentally the formation of alloy cementite and its enrichment with the alloying element, particularly at elevated temperatures. In this case, the excess phase will manifest itself as a special carbide. It is possible that, during the first stages of decomposition, intermetallic compounds separate out from the super-cooled Card3/5 austenite (in the case of Ni, Cr and V steels)

SOV/129-59-2-4/16

Carbide Formation During Isothermal Decomposition of Alloyed Austenite in Hypereutectoidal Steels

During the main decomposition of the austenite, the alloying elements continue to separate out of the solid solution in the form of excess special carbides and alloy cementite and they can also be dissolved in the cementite which is contained in the eutectoid. Apparently at 350 °C the separation of the carbide phase and its formation proceeds in the same sequence as it does at 600 °C but the intensity and the degree of completion of these processes are lower in this case. From the point of view of increase in intensity of the final transition from the austenite into the carbide phase, the alloying elements of the investigated steels can be classified approximately in the following order: a) at 600 °C - Ni. Min. Cr. W. V. Mo; b) at 350 °C - Min. Ni. V. Cr. W. Mo. As regards the intensity of rejection in the excess carbides, these alloying elements can be classified for both temperatures in the following sequence: Min. Ni. V. Cr. W. Mo. The quantity of alloying elements which remain dissolved in the ferrite is considerably larger in the case of

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Carbide Formation During Isothermal Decomposition of Alloyed
Austenite in Hypereutectoidal Steels

decomposition at 350 °C (particularly for Mn and V).

Nickel appears to be a non-carbide forming element and is
Nickel appears to be a non-carbide forming element and is
observed to a slight extent in the excess cementite
but there is no nickel in the pearlitic carbide.
There are 1 figure, 1 table and 3 references, 1 of which
is Soviet, 1 German and 1 Japanese.

ASSOCIATION: Leningradskiy tekhnologicheskiy institut imeni
Lensoveta (Leningrad Technological Institute
imeni Lensovet)

Card 5/5

2208, 2808, 2515

s/080/60/033/012/012/024 D209/D305

1.2400 AUTHORS:

I.

Anitov, I.S., and Maksimova, A.G.

Galvano-diffusion brazing of titanium

PERIODICAL: Zhurnal prikladnoy khimii, v. 33, no. 12, 1960,

2724 - 2728

TEXT: Titanium is an excellent constructional material for many applications, but its low antifriction properties set it at a disadvantage and the present work was carried out in order to obtain firmly adhering brass layers on the surface of the titanium. Brass plating from cyanide solutions was not successful, so the possibility of using a galvano-diffusion method was investigated. The principle is to deposit a layer of copper of the required thickness on the titanium and then to fire the parts in a medium containing the vapors of volatile compounds of zinc, the copper being saturated with zinc to produce brass. Technically pure titanium mark VT--1, produced in a vacuum arc furnace was used, and the ingots weighing 50 kg were forged into billets from which samples for tes-Card 1/3

### "APPROVED FOR RELEASE: 04/03/2001

### CIA-RDP86-00513R000101630006-4

25657 S/080/60/033/012/012/024 D209/D305

Galvano-diffusion brazing ...

ting of dia. 10 mm and length 15 mm were cut. The work consisted of the following basic steps: 1) Preparation of the surface of the tintended for the following basic steps: 1) Preparation on the surface of the tintended for the compound to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of volatile zinc compounds to produce brase. Being in the vapors of the lime and washed with water. The best etching solution was found to be concentrated with water. The best etching solution was found to be concentrated hydrochloric acid at 50°. For galvanic deposition of copper the hydrochloric acid at 50°. For galvanic deposition of copper the standard acid electrolyte used was  $\text{CuSO}_4$  of  $\text{5H}_2\text{O} = 200-250 \text{ g/l}$ ,  $\text{H}_2\text{SO}_4 = 50-75 \text{ g/l}$ , temperature  $18-20^\circ$  and current density 1-2 A/l

 $^{-2^{-4}}$  dm². To obtain copper coatings of thickness greater than 30-40  $\mu$ , dm². To obtain copper coatings of thickness greater than 30-40  $\mu$ , it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was necessary to do the work in two stages. First, the etched it was nece

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25657 \$/080/60/033/012/012/024 D209/D305

Galvano-diffusion brazing ...

fire-clay, ferro-silicon and ammonium chloride, the amount of which was calculated from the weight of copper deposited. Quite satisfactory results were obtained by firing at  $730-750^{\circ}$  for 6 hours, the copper layers 1.0 mm thick being almost completely brazed. The microstructure of the brazed layer (firing conditions  $750^{\circ}$  for 6 hours) is shown. It is clear that  $(\alpha + \beta)$  brass is formed with transition layers on the Cu-Ti boundary. Friction testing was carried out on the Amsler machine with a rate of sliding of 0.4 m/sec. and with varying specific loads, from 15 to 100 kg/cm² using continuous lubrication. There are 3 figures and 2 references: 1 Sov-Viet-bloc and 1 non-Soviet-bloc.

SUBMITTED: January 7, 1960

Card 3/3

1413, 1416, 2808, 4016

26861 3/080/61/034/004/002/012 A057/A129

18.8300

Anitov, I.S., Gorbunov, S. A.

TITLE :

AUTHORS:

Oxidation of titanium and its alloys in air at high temperatures

PERIODICAL:

Zhurnal prikladnoy khimii, v. 34, no. 4, 1961, 725 - 734

The oxidation behavior of commercial-grade titanium and binary titanium alloys with 5 % aluminum, tin, copper, silicon, iron, chromium, molybdenum or vanadium, and with 1.5 % and 10 % vanadium, respectively, were investigated at 700 - 1,000°C in untreated laboratory air. Some general considerations on the influence of these elements on titanium oxidation are presented. In spite of many investigations related to titanium oxidation, such as works by P. Kofstad et al. (Ref. 3: Acta Chem. Scand., 12, 239, 1958), O. Kubaschewskiy and B. Hopkins, V. I. Arkharov and G. P. Luchkin (Ref. 5: DAN SSSR, 83(6), 837, 1952, and W. Kinna and W. Knorr (Ref. 6: Z. Metallk., 47, 8, 594, 1956) few data are published concerning the influence of the alloy elements. Oxidation of titanium is rather complex, since it obeys in the range 300 - 600°C the cubic rate law, at 650 - 850°C the parabolic rate law, and above 800-850°C the linear rate law,

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### "APPROVED FOR RELEASE: 04/03/2001

CIA-RDP86-00513R000101630006-4

26861 8/080/61/034/004/002/012 A057/A129

Oxidation rate of titanium .....

due to the effect of scale formation. Different data were also published on oxidation of titanium in oxygen and air atmosphere. A. D. Makkvillen and M. K. Makkvillen (Ref. 1: Titan (Titanium), Metallurgizdat, 1958) assume that the effect of alloy elements on scale formation should be considered on the basis of Wagner's diffusion theory. TiO2 formed on the surface during oxidation could be considered as semi-conductor with a defiency in anions. Substitution of titanium ions in TiO2 by ions of metals with lower valency should cause an increase in electroconductivity and diffusion rate; an opposite effect should have metal ions with higher valency than titanium. Corresponding observations were made by K. Hauffe et al. (Ref. 9: Elektro-chem., 56, 937, 1952). The alloys investigated in the present work were prepared by double re-melting of a Tro (TGO) titanium sponge. The used titanium and alloys contained the following impurities: up to 0.20 % iron, 0.08 % silicon, 0.05 % carbon, 0.06 % chlorine, 0.03 % nitrogen, 0.15 % oxygen, 0.012 % hydrogen. Oxidation rate was studied at 700, 800, 900, and 1,000°C by the gravimetric method, at durations of the test of up to 45 hours. Oxidation of pure titanium in air occurs according to the parabolic rate law (Figure 1), just at the initial period the oxidation rate deviates from it (at 700°C in the first 3 hours oxidation occurs almost by the cubic rate law). The

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Oxidation rate of titanium ....

change to linearity at 900°C after 45 hours is explained by destruction of the scale. This occurs probably also at 1,000°C oxidation, but there (corresponding to observations by Ref. 3) impurities effect a quick sintering of scale. Results (Figures 2 - 5) on the effect of 5 % admixtures of alloy elements demonstrate that aluminum and silicon decrease the oxidation rate in the whole range of test temperatures. Iron, molybdenum, and vanadium increase the oxidation rate, the latter tow especially at 1,000°C (Figure 5). While at 1,000°C oxidation of pure titanium the parabolic rate law was observed, 5 % vanadium admixtures effect a change to the linear rate law after 3 hours of oxidation and thus a strong increase in the oxidation rate. An analogous effect is observed with molybdenum admixtures at 1,000°G. Hence these admixtures apparently prevent sintering of scale at 1,000°C oxidation. According to Kubaschewski and Hopkins, as well as Leslie and Fontana, Cr/Ni alloys with high molybdenum content show a "eatastrophic" oxidation. The latter is explained by the formation of volatile MoO3. Among others, G. Ratheanan and J. Meijering (Ref. 11: Metallurgiya, 42, 167, 1950) agree with this hypothesis. Apparently in the present work the formation of low-melting, volatile MoO<sub>3</sub> or V<sub>2</sub>O<sub>5</sub> (in vanadium alloys) effects the observed "catastrophic" oxidation of titanium at 1,000°C. Oxidation rate curves of other

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# "APPROVED FOR RELEASE: 04/03/2001

CIA-RDP86-00513R000101630006-4

26861 3/080/61/034/004/002/012 A057/A129

Oxidation rate of titanium :...

alloys for 1,000°C demonstrate that 5% copper alloys oxidize according to the cubic rate law, while for 5% iron and 5% tin alloys, this rate law is reached after 5 - 10 hours of oxidation. This somehow unexpected result can be explained by the influence of the nature of the oxides formed. Decrease of oxidation rate effected by aluminum and silicon, i.e., occurrence of the oxidation according to the cubic rate law with 5 % admixtures of these elements indicates that oxide films of these alloys yield a good protection from oxygen diffusion into the metal. Hence aluminum and silicon admixtures to titanium cause a shift of oxidation kinetics towards lower temperatures (200 - 300°C lower than for pure titanium), i.e., aluminum and silicon increase the heat resistance of titanium alloys. In Figure 2 and 3 it is shown that copper causes at 700° and 800°C an increase, and at 900° and 1,000°C (Figure 4,5) a decrease of oxidation rate compared to pure titanium. Tin has little or no effect on titanium oxidation. Summarizing it can be said: Aluminum and silicon decrease, while vanadium, iron and chromium increase the oxidation rate of titanium in the whole investigated temperature range. Copper effects an increase at lower and a decrease of oxidation rate at higher temperatures, while molybdenum shows the opposite effect. Tin has practically no effect on titanium oxidation. Above certain temperatures vanadium and molybdenum effect "catastrophic" oxidation of titanium. Thus, in first ap-

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Oxidation rate of titanium ....

proximation, it seems that the hypothesis made by Ref. 1 related to substitution of titanium ions is valuable. But a more detailed analysis of the present results demonstrates considerable deviations from this rule. The present authors consider that also other factors influence titanium oxidation. For instance, properties of the formed scale the effect of alloy elements on the formation of scale and the oxygen-saturated layer below the scale are affecting the titanium oxidation rate. These effects have to be investigated separately for each of the elements. In connection with "catastrophic" titanium oxidation alloys containing 1.5 % and 10 % vanadium, respectively, were investigated. The obtained results (Pigures 6 - 9) demonstrate at 1,000°C for 5 % and 10 % vanadium alloys, and at 800 and 900°C for 10 % vanadium alloys a linear oxidation rate law, otherwise a parabolic rate law. The change to the linear rate law (800°C for 10 % vanadium and 1,000°C for 5 % vanadium) alloy indicates the beginning of "catastrophic" oxidation. Increase in vanadium content increases the oxidation rate at all investigated temperatures. Thus with increasing vanadium content the temperature of "catastrophic"oxidation also decreases (from 1,000°C with 5 % V to 800°C with 10 % V). Catastrophic oxidation occurs when volatile vanadium pentoxide melts and evaporates in the scale (oxide film). At lower temperatures apparently a spinel structure is formed, and thus melting of  $V_2 O_5$  is more difficult. The Card 5/14

# "APPROVED FOR RELEASE: 04/03/2001

CIA-RDP86-00513R000101630006-4

26861 9/080/61/034/004/002/018 A057/A129

Oxidation rate of titanium ....

character of the form of vanadium-titunium alloy samples after exidation at different temperatures is similar and indicates the prevailing diffusion of oxygen through the oxide film. The scale is formed principally in the phase interface metal-oxide. One of the factors effecting the destruction of the oxide film is the different molar volume of vanadium pentoxide and rutile. The present authors point out that in various technological operations the effect of vanadium on titanium oxidation must be considered. There are 11 figures and 11 references: 4 Soviet-bloc and 7 non-Soviet-bloc.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut neftekhimicheskikh

protsessov (All-Union Scientific Research Institute of Petrochemi-

cal Processes).

SUBMITTED:

July 23, 1960

Card 6/14

30197

S/080/61/034/011/010/020 D243/D301

18 8300

Anitov, I.S., and Kukalenko, B.D.

AUTHORS:

TITLE:

The effect of thermal processing on the corrosion resistance of the titanium alloy BT3-1 (VTZ-1) in

sulphuric acid solutions

PERIODICAL:

Zhurnal prikladnoy khimii, v. 34, no. 11, 1961,

2466 - 2472

TEXT: The authors state that the corrosion of thermally processed alloys has not been previously studied. They set out to examine the effect of thermal processing of an  $\alpha+\beta$  titanium alloy on corresion resistance in H<sub>2</sub>SO<sub>4</sub> solutions and to detect any link bet-

ween the alloy's structure and corrosion properties. To this end samples of VTZ-1 titanium (aluminum 6 %, molybdenum 8 %, chromium 5 %) were subjected to various thermal processing regimes. As corroding medium they used 25 % and 75 %  $\rm H_2SO_4$ , in whose concentrati-

ons the corrosion rate of titanium is the highest, according to V. V. Andreyeva, and V.N. Kazarin (Ref. 1: DAN SSSR, 121, 5, 1958). Card 1/3

5/080/61/034/011/010/020 30197 The majority of trials were carried out at 22-24°C with a few at 12-1400. Three or four specimens were used for a single trial us D243/D301 The majority of trials were carried out at 22-24 U with a lew at 12-1400. Three or four specimens were used for a single trial, using 12-1400. Three or four specimens were mapping remained in 25 % The effect of thermal processing ... ing 300-400 ml. solution per sample. The samples remained in 25 % ing 500-400 ml. solution per sample. The samples remained in 70 % u so for AR hours. Correction was u so for AR hours. ing 200-400 mi. Bolution per sample. The samples remained in 22 % H<sub>2</sub>SO<sub>4</sub> for 260 hours and in 72 % H<sub>2</sub>SO<sub>4</sub> for 48 hours. Corrosion was estimated from external appearance, duration of passivity and loss of weight (am/) mm2/hr appearance over whole test neriod with corestimated from external appearance, duration of passivity and form of weight (gm/l mm2/hr calculated over whole test period weight (gm/l mm2/hr calculated over whole test period for measivity period). Maximum scatter of data for weight rection for passivity period). vergue (gm/1 mm-/nr carculated over whose test person weight rection for passivity period). Maximum scatter of data for weight rection for passivity period). Maximum scatter of data for weight rection for passivity period). 1088; under equivalent conditions, was approximately 10 %. The structure of the samples was attudied with onticel (veno) and e toss, under equivalent conditions, was approximately to %. The structure of the samples was studied with optical (x500) and electron (x10,000) microscopes. It was found that thermal processing tron (x10,000) microscopes. It was found that thermal processing had a marked effect on the corrector registering of unx-1 titerius had a marked effect on the corrosion resistance of VTZ-1 titanium and a marked effect on the corrosion resistance of very serior of nosed and in 25 % H SO as about hy the change in the named of nosed allow in 25 % H SO as about hy the change in the named of nosed allows in 25 % H SO as about hy the change in the named of nosed allows in 25 % H SO as about hy the change in the named of nosed allows in 25 % H SO as about hy the change in the named of nosed allows in 25 % H SO as about hy the change in the named of named and the named of named and the named of named and named and the named of named and nad a marked effect on the corrosion resistance of VID-1 titalium alloy in 25 % H<sub>2</sub>SO<sub>4</sub> as shown by the change in the period of passivity and corrosion rate of the alloy. This effect was linked with nature of the degree of heterogeneity nature of structural differences e.g. the degree of heterogeneity, nature of the dispersion phases and the state of strain of the allow the dispersion phases and the state of strain of the allow the dispersion phases and the state of strain of the allow the dispersion phases and the state of strain of the allow the dispersion phases and the state of strain of the allow the dispersion phases and the state of strain of the allow the state of strain of the state of strain of strain of strain of state of strain of state of stat the dispersion phases and the state of strain of the siloy, manufacture properties of the natural ovide film deserted moinly the dispersion phases and the state of strain of the garage and the state of strain of the matural oxide film depended mainly on protective properties of the natural oxide film depended mainly of the heterogeneity of the atructure. The period of passivity diministrate the heterogeneity of the atructure. protective properties of the natural oxide illm depended mainly on the heterogeneity of the structure, the period of passivity diminities the heterogeneity of the structure, single phase or coarsely beteroconstable with coarsely atmost the period of passivity diminities. the neterogeneity of the structure, the period of passivity diminicard 2/3

30197 The effect of thermal processing ... \$/080/61/034/011/010/020 ous alloys had the highest corrosion resistance which was also increased by an  $\alpha$  +  $\alpha$ ' dispersion mixture or states of strain.  $\omega$ -phase had no effect. At 12-14°C, the corrosion rate was much lower, in 75 % H<sub>2</sub>SO<sub>4</sub> corrosion proceeds much more rapidly largely because of a decrease in the passivity period. There are 5 figures, 2 SUBMITTED: January 7, 1961 Card 3/3

1,2250

5/126/62/014/004/017/017 E073/E535

**AUTHORS:** TITLE:

Mozhayev, S.S., Sokiryanskiy, L.F. and Anitov, I.S. On the mechanism of high-temperature oxidation of

PERIODICAL: Fizika metallov i metallovedeniye, v.14, no.4, 1962,

TEXT: G. Wallwork and A. J. Jenkins (J. Electrochem. Soc., 1959,  $\underline{106}$ , (1), 10) explain the transition from the parabolic law of oxidation to the linear law by means of the hypothesis according to which the rate of oxidation is controlled by the gradient of oxygen concentration in the metallic base of the specimen and he assumed that, at the end of the parabolic oxidation period, the gradient reaches a steady-state value and, as a result, the rate of oxidation remains constant. J. Stringer (Acta met., 1960, 8, 11, 758) found that during oxidation at 950°C according to the parabolic law about 45% of the entire oxygen absorbed by the titanium is dissolved in the core of the specimen, whilst at the end of the linear oxidation section only 5% is dissolved. Analysis of experimental data available to the authors of this Card 1/3

On the mechanism of high-temperature ...S/126/62/014/004/017/017 E073/E535

paper indicates that during transition from the parabolic to the linear oxidation law, the rate of scale formation increases appreciably but no appreciable changes were found in the kinetics of dissolution of oxygen in the metal. of scale formation, the ratio between the quantity of oxygen which is chemically combined and the oxygen which is dissolved in the metal changes. However, since in the "linear" range the absolute quantity of the oxygen dissolved in the metal continues to increase with the progress of time, the depth of penetration of the oxygen into the titanium must increase. This was confirmed by microhardness measurements of specimens which were subjected to oxidation at 900°C for periods between 0.5 and 16 hours. the specimens were exposed to oxidation over a long period so as to ensure transition into the linear range, after which the scale was removed and the specimens were subjected to a second oxidation at the same temperature. in the metallic core would be the factor controlling the rate of If the gradient of oxygen concentration oxidation, the repeated oxidation would have to proceed in accordance with the linear law. However, the new curves of the

On the mechanism of high-temperature ... S/126/62/014/004/017/017 E073/E535

total weight increment, although somewhat lower, had exactly the same character, i.e. at first, oxidation was in accordance with a parabolic law and then in accordance with a linear law. Thus, the obtained experimental results are not in agreement with the hypothesis of Wallwork and Jenkins, who associated the transition from the parabolic to the linear law with the formation in the surface layer of the metal of a saturated zone with a constant gradient of oxygen concentration. This transition is due to processes which develop in the oxide film itself and, therefore, further investigations should be directed towards the study of the properties and structure of this film. There are 2 figures. SUBMITTED:

May 16, 1962

Card 3/3

ACCESSION NR: AT4007031

S/2598/63/000/010/0100/0107

AUTHOR: Gorbunov, S. A.; Anitov, I. S.

TITLE: Kinetics of oxidation of commercial grade titanium at high temperatures in air

SOURCE: AN SSSR. Institut metallurgii. Titan i yego splavy\*, no. 10, 1963. Issledovaniya titanovy\*kh splavov, 100-107

TOPIC TAGS: titanium oxidation, high temperature oxidation, scale structure, oxide layer structure, titanium oxidation kinetics, titanium oxidation mechanism

ABSTRACT: Oxidation of commercially pure titanium in mented laboratory (undried) air was studied at constant temperatures of 800-1200 C. The oxidation mechanism has been elicited by investigating the comparative O<sub>2</sub> distribution in the oxide layer and in the contaminated Ti zone situated beneath it, the thickness of the gas-contaminated surface, measured with a PMT-3 apparatus under 50 g load (no further details given), and the thickness and structure of the oxide scale after sintering (structural analysis by X-ray). The oxidation mechanism from 1100-1200 C differs from that at 800-1000 C principally in the higher diffusion rate of Ti atoms toward the surface. Further, at 1100-1200 C, O<sub>2</sub> distribution differs between the oxide scale layer and the air-contaminated layer. The oxidation rate measured up to 32

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### "APPROVED FOR RELEASE: 04/03/2001

#### CIA-RDP86-00513R000101630006-4

ACCESSION NR: AT4007031

hours, changes from linear (800, 900 C) to parabolic (1000 C) to cubic in nature (1100, 1200 C) with 4-hour experimental values at these five temperatures, of 10, 40, 220, 280 and 460 g/m<sup>2</sup>, respectively. The air contaminated Ti layer is characterized by a thin alpha-Ti shell of high hardness owing to high  $O_2$  content, underlaid by up to several mm of beta-Ti of lesser hardness and an  $O_2$  content of 0.15-2%. "G. P. Nadutenko also took part in the work." Orig. art. has: 3 tables and 5 graphs.

ASSOCIATION: Institut metallurgii AN SSSR (Metallurgical Institute AN SSSR)

SUBMITTED: 00

DATE ACQ: 27Dec64

ENCL: 00

SUB CODE: MM

NO REF SOV: 002

OTHER: 005

Card 2/2

ACCESSION NR: AP4039277 S/0148/64/000/005/0135/0139 . AUTHORS: Anitov, I.S.; Kukalenko, B.D. TITLE: The effect of heat treatment on the corrosion resistance of SOURCE: IVUZ. Chernaya metallurgiya, no. 5, 1964, 135-139 TOPIC TAGS: heat treatment, corrosion resistance, Ti alloy, mechani-ABSTRACT: The authors studied the effects of heat treatment on the mechanical properties of type  $\alpha+\beta$ -Ti-alloy and its corrosion resistance. The specimens were widely used "VTZ-1" Ti-alloy specimens sistance. The specimens were widely used "VTZ-1" T1-alloy specimens which contained 6% Al, 3% Mo and 3% Cr. They were prepared by 800C annealing of 16 mm diam.rods. The heat treatment temperatures were followed by normalizing and water quenching. Cylinders with a 12-15 mm diam.and a height of 20-22 mm were cut out. A 25% solution of sulfuric acid was used for corrosion tests at 20-24C and 12-15C.

The specimens remained in the medium from 260 to 1000 hrs. Ultimate

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R000101630006-4"

The specimens remained in the medium from 260 to 1000 hrs. Ultimate

ACCESSION NR: AP4039277

strength and hardness increased with tempering temperatures up to 5000 while plasticity was equal to zero in all tests. The rate of corrosion dropped with raised heat treatment temperatures and at 11000 corrosion attack was negligible. Thermal oxidation enhanced corrosion resistance substantially. Heat treatment affected the structure and strength of the natural passivating exide film formed by special air heating at temperatures above 6000 as well as the strength of the material. Although tempering at 300-4000 had negligible effect on the structure after hardening, the rate of corrosion of tempered specimens was lower than that of hardened specimens because of the relief of cooling stresses. In high-hardness alloys (normalizing and quenching from 10500 followed by has: 4 figures

ASSOCIATION: Leningradskiy tekhnologichoskiy institut (Leningrad Institute of Technology)

SUBMITTED: 03May63

SUB CODE: MM

Card 2/2

NR ILEF SOV: 002

ENCL: 00 OTHER: 000

-	ACC NR: AT6012384  AUTHORS: Nadutenko, G. P.; Gorbunov, S. A.; Anitov, I. S.; Teodorovich, V. P. & ORG: none	
	16	
	TITLE: A study of the effect of nickel, silicon, and niobium on the oxidation of	
	SOURCE: Soveshchaniye po metallokhimii, metallovedeniyu i primeneniyu titana i yego alloys); trudy soveshchaniya. Moscow, Izd-vo Nauka, 1965, 148-154	
	TOPIC TAGS: titanium, titanium alloy, thermal stability, corrosion resistance, nickel,	
	ABSTRACT: The oxidation in air of binary titanium alloys is studied at a temperature 25% niobium. The alloys were prepared by double melting of electroder in an arc vacuum furnace. The new prepared by double melting of electroder in a state of the stat	
	arc vacuum furnace. The oxidation kinetics were studied by the method of periodic weighing. The specimens were heated in air for up to 16 hrs at 8001000C and up to 8 hrs at 11001200C. It was found that 1.5% Si in the alloy was optimum for Cord 1/2	

L 30370-66							
increasing the therm increase in the Si quintroduction of Ni cunalloyed titanium.	pntent decreases considerably re-	ses the oxid educes the t tion of 25%	ation resistan hermal stabili Nb vonv greatl	ce on t ty as c y incre	compared wi eases the t	th hermal	· 0
l table. SUB CODE: 11/	SUBM DATE:	O2Dec65/	ORIG REF:	010/	OTH REF:	001	
·		·			•	•	
Card 2/2 (1 C							
	7,1				2		q

ACC NR: AP7005133 SOURCE CODE: UR/0126/66/022/004/0591/0597 AUTHOR: Lerinman, R. M.; Khvostyntsev, K. I.; Nikanorov, M. A.; Anitov, I. S.; Ksenofontova, T. B. ORG: Institute of Metal Physics, AN SSSR (Institut fiziki metallov AN SSSR) TITLE: Combined effect of plastic deformation and aging on the structure and properties of SOURCE: Fizika metallov i metallovedeniye, v. 22, no. 4, 1966, 591-597 TOPIC TAGS: titanium alloy, metal aging, plastic deformation, phase composition, metal recrystallization / TS6 titanium alloy ABSTRACT: The effect of plastic deformation (rolling with degrees of deformation amounting to 3, 10 and 40% and aging(at 480°C for 2, 10, 30 and 100 hr) on the fine structure (the kinetics of decomposition of the  $\beta$ -phase, dispersity and the distribution of the  $\alpha$ -phase) of TS6 titanium alloy (3.22% Al, 3.42% Mo, 7.80% V, 10.80% Cr, 0.18% Fe, 0.03% C, 0.01% Si, 0.07% O<sub>2</sub>, 0.011%  $\,\mathrm{N}_{2}^{}$ , with Ti as the remainder) was investigated by means regular and electron microscopy and measurements of hardness and tensile strength. It is shown that plastic deformation accelerates the decomposition of the metastable  $\beta$ -phase and results in a more fine-

**APPROVED FOR RELEASE: 04/03/2001** CIA-RDP86-00513R000101630006-4"

UDC: 548.526

Card

ACC NR1 AP7005133

-grained and uniform structure devoid of undecomposed boundary-layer and intragranular residues of the β-phase, which, together with the high dogree of dispersity of the particles of the segregating α-phase, leads to a general improvement in mechanical properties. Quenching the alloy from 800°C following 3% deformation results in polygonization; following 10% deformation, in partial recrystallization; and following 40% deformation, in total recrystallization of the structure. In this last case, since the decomposition of the recrystallized β-phase occurs slowly, a marked change in the alloy's hardness is observed only after 100 hr of aging at 480°C. This may be a cause of the heterogeneity of the alloy's properties following its hardening by heat treatment. The highest hardening rates were observed for the specimens subjected to 3 and 10% deformation prior to their quenching, which indicates that an incompletely recrystallized structure is favorable to the increase in mechanical strength following aging. Orig. art. has: 7 figures, 3 tables.

SUB CODE: 20/ SUBM DATE: 05Feb66/ CRIG REF: 001/ OTH REF: 001

Card 2/2

ACCESSION NR: AP4018858

8/0043/64/000/001/0005/0014

AUTHOR: Anitova, Ye. S.

TITLE: The restricted nature of solutions of a system of third-order differential equations

SOURCE: Loningrad. Universitet. Vestnik. Seriya matematiki, mekhaniki i astronomii, no. 1, 1964, 5-14.

TOPIC TAGS: differential equation, third order differential equation, Hurwitz condition, dissipative system

ABSTRACT: The author has investigated the restricted nature, as  $t \rightarrow \infty$ , of the solutions of the system of differential equations:

$$\frac{dx}{dt} = a_{11}x + a_{12}y + a_{12}z + p_1(t, x, y, z), 
\frac{dy}{dt} = f(x) + a_{21}y + a_{22}z + p_2(t, x, y, z), 
\frac{dz}{dt} = a_{21}x + a_{21}y + a_{22}z + p_3(t, x, y, z),$$
(1)

Card 1/3

ACCESSION NR: AP4018858

where  $a_{ij}$  are constants, f(x) and  $p_i(t,x,y,z)$  (i=1,2,3) are continuous and ensure the unuiqueness of the solution for all x,y,z,t; f(x) satisfies the generalized Hurwitz condition:  $ax^2 < xf(x) < \theta | x^2$  when  $|x| \ge 1$  (where  $\alpha$  and  $\beta$  are the limits for the variation of parameter a). Under these conditions, the roots of the characteristic equation of the linear system corresponding to (1) all have negative real parts. It is assumed that all the perturbing functions  $p_i(t,x,y,z)$  are in modulus less than some constant M>0 for all x,y,z,t. After some manipulations and changes of notation, system (1) is put into the form:

d changes of notation, system (1) is put into the notation,
$$\frac{dx}{dt} = y - x + p_1(t, x, y, z),$$

$$\frac{dy}{dt} = z - f(x) + p_2(t, x, y, z),$$

$$\frac{dz}{dt} = -ax - bf(x) + p_2(t, x, y, z),$$
(2)

for which the Hurwitz conditions are:

$$a+b\frac{f(x)}{x}>0$$
 при  $|x|>1$ ,  
 $(1-b)\frac{f(x)}{x}-a>0$  при  $|x|>1$ . (3)

Card 2/3

# ACCESSION NR: AP4018858

In system (2), seven different cases are distinguished depending on the natures of a and b. The author then considers the solution of four of these cases. She derives sufficient conditions for the dissipativity and for the existence of periodic solutions when the  $p_i(t,x,y,z)$  are periodic. A system is said to be dissipative if there exists a bounded region such that all solutions of the system enter into this region as  $t \to \infty$  at some time and remain there from then on. Orig. art. has: numerous conditions.

ASSOCIATION: None

SUBMITTED: 03Dec62

DATE ACQ: 23Mar64

ENCL: 00

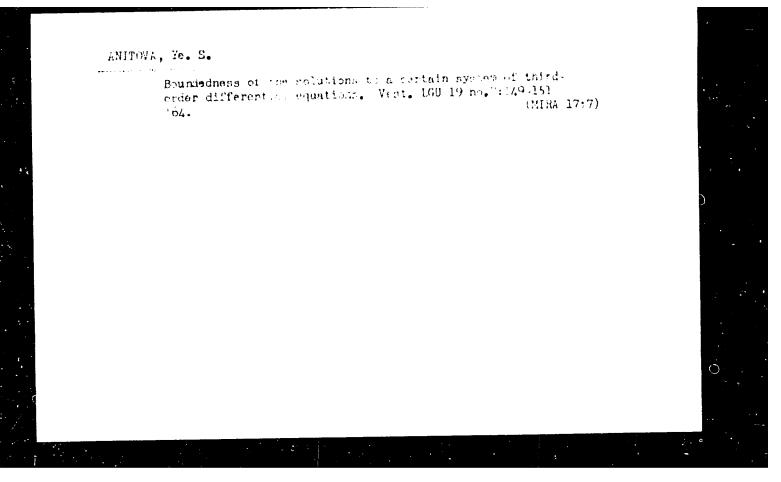
SUB CODE: MM

NO REF SOV: 005

OTHER: 002

3/3

Card



s/020/62/145/003/001/013 B172/B112

AUTHOR:

Anitshchenko, R. I.

TITLE:

A boundary value problem for Thomas - Fermi and Thomas -

Fermi - Dirac equations

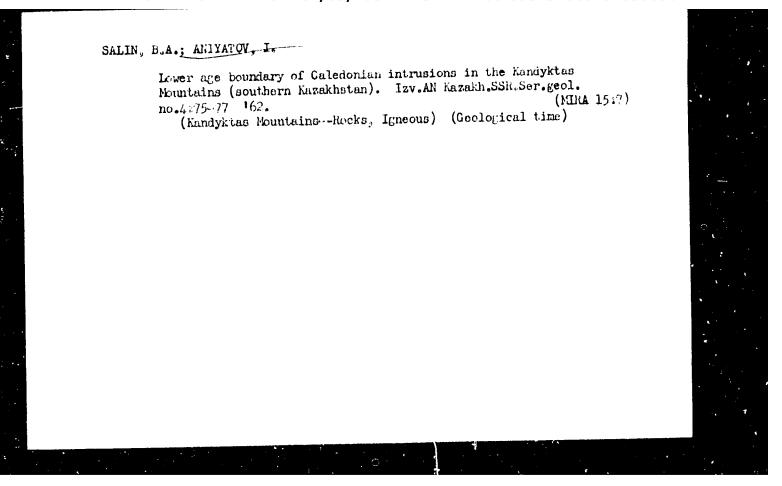
PERIODICAL:

Akademiya nauk SSSR. Doklady, v. 145, no. 3, 1962, 483-486

TEXT: Non-negative solutions are sought for the more general boundary value problem

 $\varphi''(x) = f(x, \varphi(x))\psi(x),$   $\varphi(0) = y_0, R\varphi'(R) - \varphi(R) = -q$ 

 $(y_0 > 0, q < y_0, R > 0)$  are sought. The following assumptions are made concerning the functions f(x,y) and  $\psi(x)$ : (1) f(x,y) is continuous for  $x \ge 0$ ,  $y \ge 0$ ; (2) f(x,y) increases together with y in the domain  $x \ge 0$ ,  $y \ge 0$ ; (3)  $\psi(x)$  is continuous for  $x \ge 0$ , positive for  $x \ge 0$ , and integrable on the interval [0,X] where  $X \ge 0$ ; (4)  $f(x,0) \ge 0$  for  $x \ge 0$ ; (5) f(x,y)satisfies a Lipschitz condition with respect to y in the domain  $Q > y > \alpha > 0$ , P > x > 0 for any positive  $P, Q, \alpha$ ; Card 1/2



ANIZOV, M.A.; MANULKIN, Z.M.; TATARENKO, A.N.

Tashkent Pharmaceutical Institute is 25 years old. Uzb.khim.
zhur. 6 no.518~88 '62. (MIRA 15:12)

1. Tashkentskiy fermatsevticheskiy institut.
(TASHKENT—PHARMACI—STUDI AND TRACHING)

#### "APPROVED FOR RELEASE: 04/03/2001

#### CIA-RDP86-00513R000101630006-4

ANNA, Dr Potor, and SALACZ, Dr Tamas, [Affiliation not given].

"Isolated Injuries of the Pancroatic Gland"

budapost, <u>Karyar Traumatologia</u>, <u>Orthopaudia os Helyroallito Sebeszot</u>,

Vol 6, do 5, 1963; pp 216-221.

Abstract [Authors' inglish summary]:

The authors describe the symptoms of isolated injuries caused by blant objects, the inchange on such injuries, their, frequency, the difficulties of their recognition, the inchange on such injuries, their, frequency, the difficulties of their recognition, in the mechanism of such injuries to such a first of the subject of the such as of common treated by the author resection should be considered to be the less of the common to the importance of the careful post-operative treatment of the patients.

[53] references, predominantly Western].

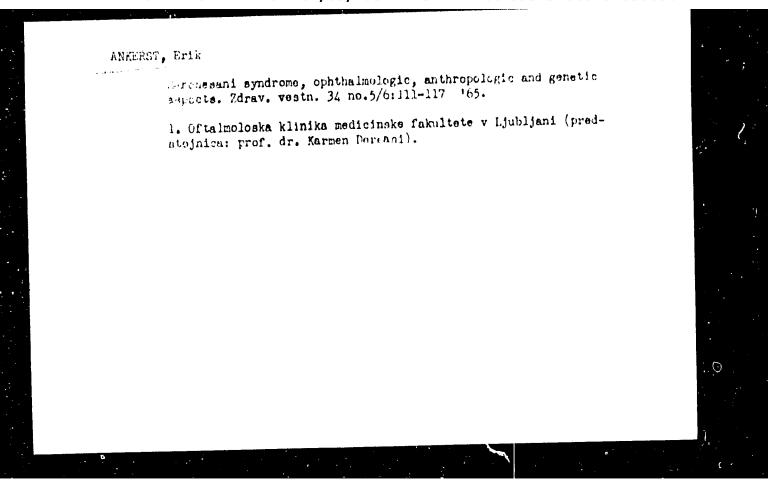
## "APPROVED FOR RELEASE: 04/03/2001

Card 1/1 /1

CIA-RDP86-00513R000101630006-4 L 46796-66 ACC NR: AP6032782 SOURCE CODE: GE/LO29/65/000/002/0083/0087 AUTHOR: Anka, Tibor M. (Budapest) ORG: none TIPIE: Effect of technology on the properties of an EAIMgGi alloy SCURCE: Neue hutte, no. 2, 1966, 83-87 TOPIC TAGS: aluminum silicon alloy, mechanical property alloy, containing smelter-aluminum EA1 99.5 with approximately 0.6% magnesium and silicon, were investigated. Best mechanical alloy properties were attained by inserting a homogenizing heating followed by quenching, and by modifying the cold-forming operation. The actual parameters of these processes depend somewhat on the plant and on the nature and end-use of the article. Data were presented for assisting in the selection of these parameters for specific purposes. Orig. art. has: 7 figures and 1 table. [JPRS: 35,398] SUB CODE: 11, 20 / SUBM DATE: 150ct65 / ORIG REF: 003 / OTH REF: 005

APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R000101630006-4"

0



ANKHEYUK, Vyacheslav Leont'yevich; IL'IN, Oleg Favlovich;
TETERINA, L.R., red.

[Automatic control of electric drives] Avtomatichesmoe upravlenie elektroprivodami. Minsk, Vyashaia shkola, 1965.
469 p. (MIRA 19:1)

S/167/59/000/006/001/002 A110/A029

13,2000

AUTHOR:

Ankhamyuk, V. L.; Ilan O. P.

TITLE:

The Synthesis of Correcting Devices of Dynamcelectric Control

Systems

PERIODICAL

Izvestiya Akademii nauk Uzbekskoy SSR, 1959, No. 6; pp. 5-19.

The modern control systems show frequently, as a consequence of different known factors, inadmissible oscillations. Therefore, the automatic control systems need correcting. i.e., stabilizing devices. The control system is composed of basic devices: devices for the given working conditions, and the correcting devices for improving the quality of transition processes. The computation of correcting devices, choosing of means of stabilization, of parameters and of the place where the stabilizing circuit is to be connected, which is combined with the calculation of the transition processes of a system under actual working conditions, is a cumbersome and complex task and does not permit an optimum solution to be found. The basic problem of the synthesis is to find easier methods of calculation. In the literature some methods are cited (Refs. 2, 3). The

Card 1/4

S/167/59/000/006/001/002 A110/A029

The Synthesis of Correcting Devices of Dynamoelectric Control Systems

article describes a technical method of a synthesis of correcting devices, which can be used when designing different control systems with one stabilization circuit. The designing of a correcting device consists of the determination, at a required quality of the control system, of the amplifulation factor and the timing constant of the stabilization circuit, of the cation factor and the choice of the means of stabilization. Criterions place of connection and the choice of the means of stabilization for the quality of the control system are: () duration of the transition for the quality of the conversion, 3) oscillation, 4) value of retarding process, 2) value of the conversion, 3) oscillation, 4) value of retarding cess is characterized by the equation

 $t_{trans} = \frac{3 \text{ to } 4}{P_{min}} \tag{1}$ 

where  $p_{min}$  is the value of the least real component of the complex solution of the characteristic equation (Ref. 1). The value of the conversion is determinable after the solution of the differential equation of the system. A minimum value is to be guaranteed. The oscillation appears as the ratio between the imaginary ( $\omega$ ) and the real ( $\mathcal{K}_{\ell}$ ) component of the

Card 2/4

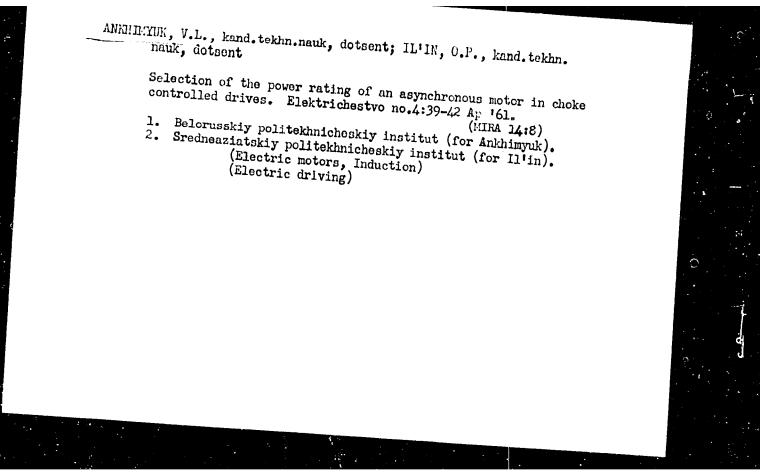
83522

S/167/59/000/006/001/002

The Synthesis of Correcting Devices of Dynamoelectric Control Systems

complex solution :  $k = w/\omega$  (2). The correcting device has to guarantee the least oscillation. The retarding torque originates in the conversion, being accompanied by the slowing down of the motor, which can lead to mechanical shocks in the transmission system (Ref. 4). The correcting device has to limit the retarding torque. Notice is to be taken of the idling. - The suggested method results in the setting up of a field of solutions in the plane of the sought pa- ..... This leads to the location of the optimum parameters (amplification factor and timing constant) of the stabilizing circuit. The amount of the conversion and of the retarding torque is determined by computation of the transition process, at chosen values of the parameters and given initial conditions. After the description of the method a general computation of a stabilizing circuit is carried out as an example of the application of this method. Differential equations are set up, which are solved and discussed. The setting up of the field of solutions is explained; a sequence of 5 points is to be obeyed. After this theoretical treatment a numerical example is given: a slabbing mill (Fig. 1) with two motors, connected in series. Each motor has a capacity of 150 kw, the generator 500 kw. Figs. 2-7 are representations of the functions and belong

Card 3/4



3/147/52/000/003/003/005/007 D236/D302

AUTHORS:

Ankhimyuk, V. D., Candidate of Tuchnical Joiences, Docent, and Sheyna, G. P., Ingineer

1:1111:

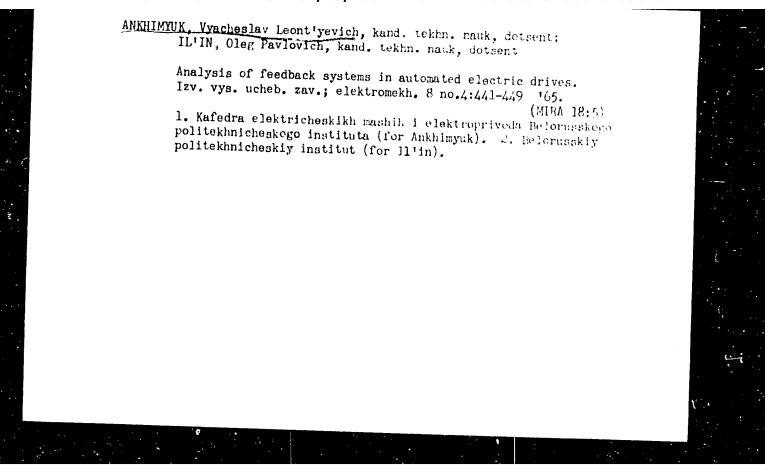
Investigating a tachemeter bridge employed an a vers-

city-type transdacer

PERIODICAL: Isvestiya vysskikh uchebnykh navedeniy. Margetika,

no. 3, 1962, 39-42

TRAT: The tachometer oridges employed in the control of industrial drives, whilst providing high-speed feedback consided with simpli-sity of design, are limited by the relative error, governed by the speed and the load on the drive. This factor lends importance to a mowledge of the conditions offering the least error ever a wide range of speed measurement. It is demonstrated from the circuit equations that the minimum relative error must be cought for each speed of rotation by determining the most favorable bridge-arm ratio on the basis of the mathematical argument. Allowing a permiss-Ourd 1/2



0-4 USSR/Farm Animals - Honey Bee. : Ref Chur - Bicl., No 1, 1959, 2752 Abs Jour : Admorten, G.D. Author : Jose w Agricultural Academy in Timiryazev Inst : Emperiment in the Acclipation of Indian Boos and Their Utilization for Pollinating Farm Crops. Title : Dokl. Rosk. s.-kh. okod. St. K.A. Timiryazeva, 1957, VVP. Orig Pub 30 di. 2, 307-310. The Parilles of Apis indica h. were obtained from China. Under conditions of the Parcel region, the Indian bees Abstract carried out flights at a temperature of approximately 990., and commenced to the out for work at a temperature 3-50 Lower than the owner Conscrations of the local bees. The rapidity of work of the Indian been is greater than Card 1/2

ANKERST, Erik
SURMANE (in cagu); Given Honeu

Country: Yugoslavia
Academic Degrees: , not given;

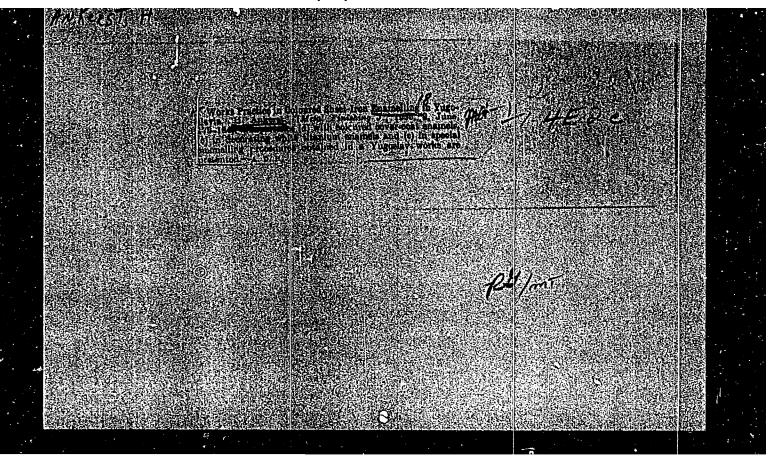
Artiliation: Eye Olinic (Oceana klinika), Ljubljana; Director (Predstojnik);

Docont Dr. Carmon DEREANI

Source: Ljubljana, Zdravstvoni vestnik, No 3-4, 1961, pp 61-67.

Data: "Morbus Besnier-Boeck-Schaumann Ophtalmologic Aspects."

"APPROVED FOR RELEASE: 04/03/2001 CIA-RDP86-00513R000101630006-4



ANKHIMYUK WA.

112-2-3417

Translation from: Referativnyy Zhurnal, Elektrotekhnika, 1957, Nr 2, p. 129 (USSR)

AUTHOR:

Ankhimyuk, V. L.

TITLE:

The Computation of Currents in an Induction-Synchronous System With Two-Zone Control (Raschet tokov asinkhronno-sinkhronnogo kaskada pri dvukhzonnom regulirovanii)

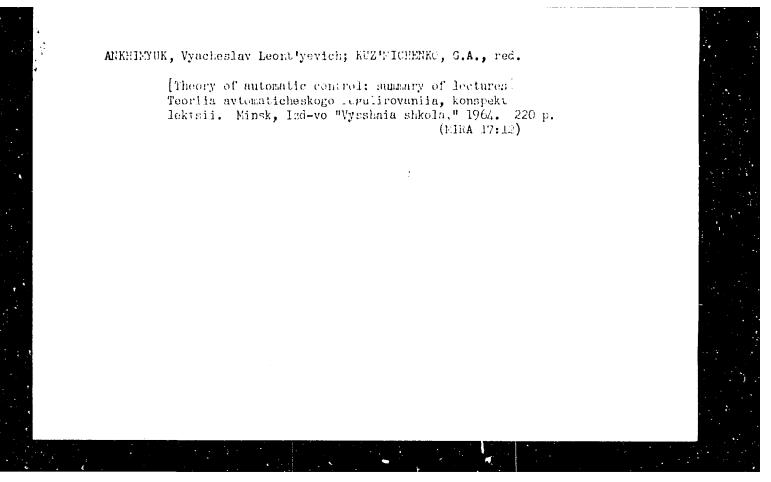
PERIODICAL: Tr. Sredneaz. politekhn. in-ta, Tashkent, Gosizdat, UzSSR, 1955, pp. 379-390

ABSTRACT:

Induction-synchronous systems (ISS), a further development of the Kramer and Scherbius Mystems are used in alternating current electric power drives of the type used for wind-tunnel blowers, mine ventillators, rolling mills, etc., where a wide range of speed control is required. The constant-power ISC consists of a main (working) induction Motor the slip energy of which is transmitted (from its slip rings) to the variable speed unit which consists of a synchronous motor and a direct current generator mounted on this motor's shaft. This generator

Card 1/2

returns the slip energy to the direct current motor which is mounted on the common shaft with the main motor. The constant-torque ISS



ANKIEWICZ, A.

"Machine Tools With Removable Cutters" p. 147. (Hechanik, Vol. 26, no. 4, Apr. 1953,
Warszawa)

So: Monthly List of Rosestan Accessions / Library of Congress, February, 1954, 1860, Uncl.

ANKIEWICZ, A.

A substitute method of manufacturing multiedged conical evolvent exles. P. 50 MECHANIK Warszawa (Stowarzyszenie Inznierow i technikow Mechanikow Polskich) Vol. 28, no. 2, February 1955

SOURCE: EEAL IC Vol. 5, no. 7, July 1956

AMERICA, A.

AMERICA, A.

AMERICA, A.

ANGERN Cornected willing machines with each messale cutters. p.245.

Vol. 29, nc. 7, July 1956. MECHANIK. Warszawa, Feland.

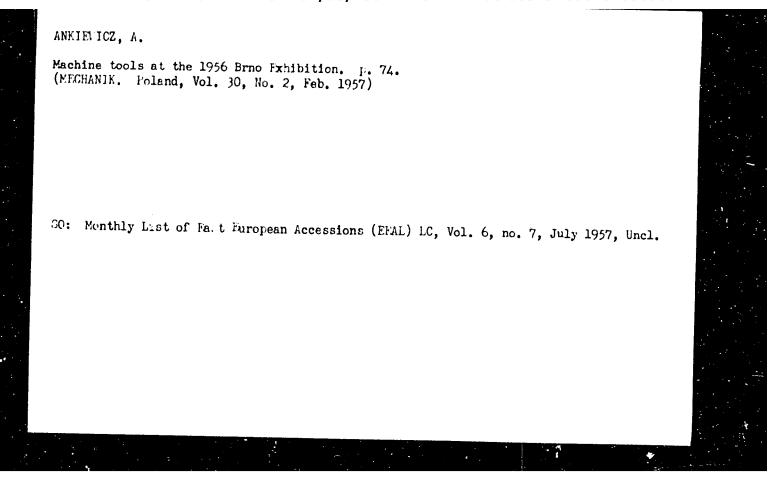
Source: East European accessions List (EEAL) Vol. 6 No. 4 April 1957

AURIS 100, 1.

New design of gear outters, p. 257.

'ECHAUTK. Warszaws, Poland. Vol. 12, nos. 1-2, 7-9, 12; Jan. Feb., July-Sept., Dec. 1957.

Monthly List of East European Accessions (MMAI) 10, Vol. 9, no. 2, Feb. 1960.



AUKIEVICE, A. ; KUNSTETTER, S.

Fresent condition of the tools nade from carbides.

F. 10. (MECHANIE) (Warszawa, Foland) Vol. 31, no. 1, Jan. 1958

30: Monthly Index of Past European Accession (EEAI) LC Vol. 7, No. 5, 1958

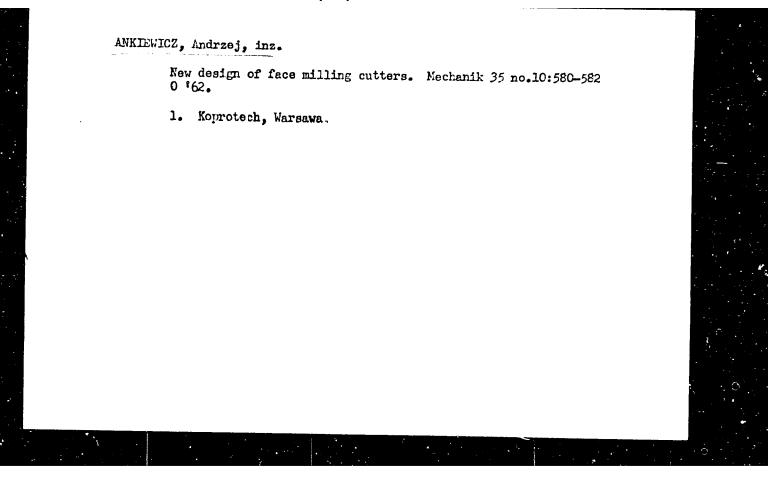
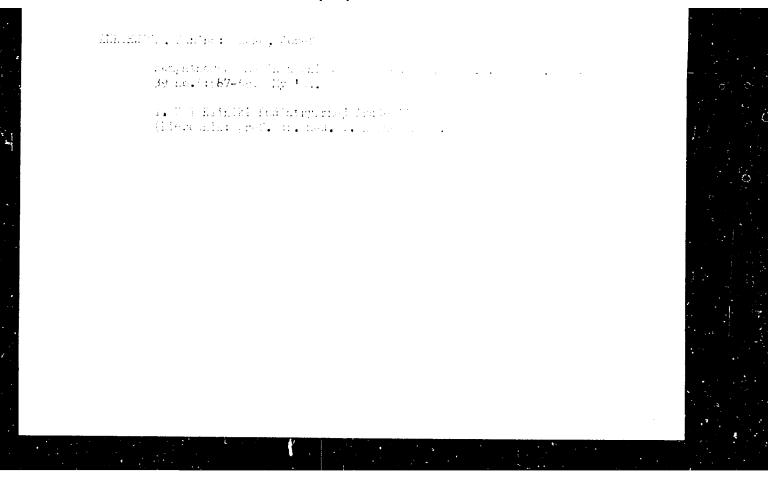
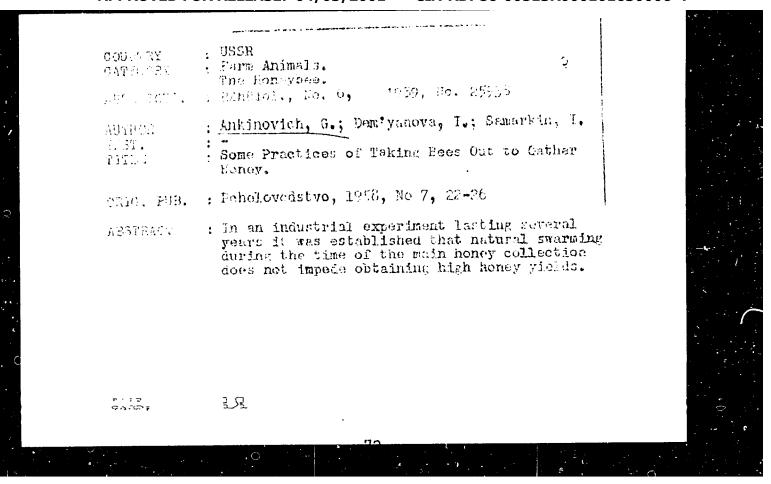


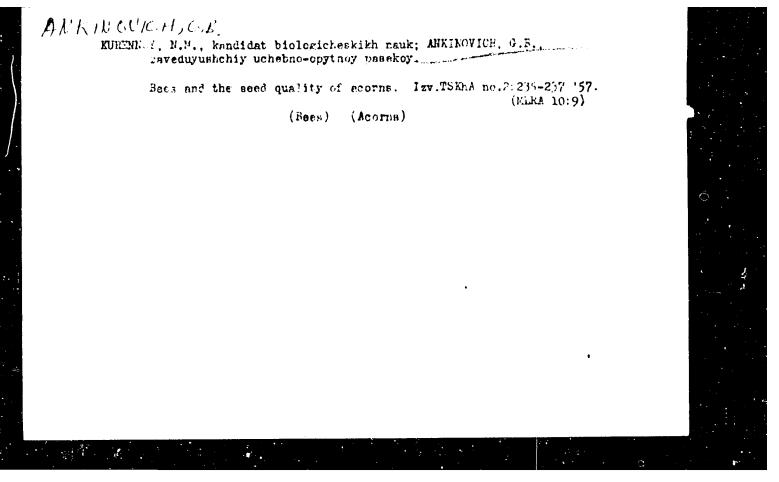
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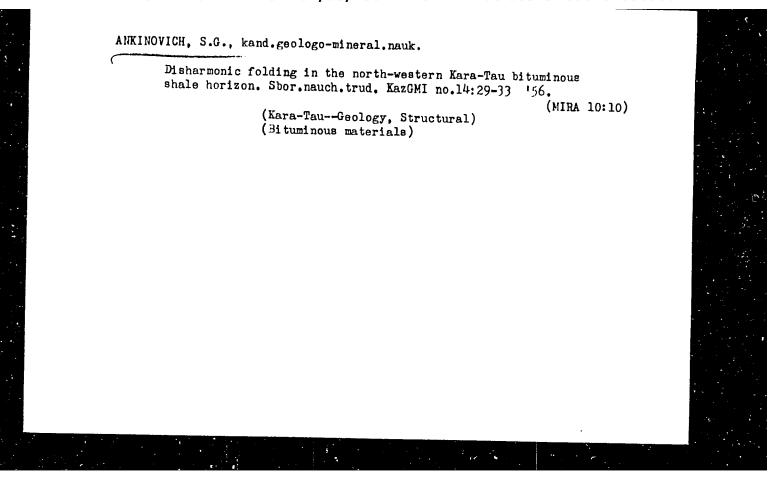
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1 U)(1) BWI(1)	
ACC NR: AP7000765 SOURCE CODE: UR/0143/66/000/005/0040/0045	
AUTHOR: Ankhimyuk, V. L. (Docent; Candidate of Technical Sciences); Il'in, O. P. (Docent; Candidate of Technical Sciences); Sheyna, G. P. (Engineer)	
ORG: Belorussian Polytechnic Institute (Belorusskiy politekhnicheskiy institut)	1.
TITLE: Selection of motors for electric drives with frequency control at constant power	
SOURCE: IVUZ. Energetika, no. 5, 1966, 40-45	
TOPIC TAGS: electric motor, frequency control	
ABSTRACT: A mothod is analyzed for selecting a motor for a system of frequency controlled drive in the P <sub>c</sub> =const operating regime. The method is based on the condition of production of a minimal size motor, in consideration of the	
problem of determining the frequencies at which the fixed range of control and power can be provided with series produced asynchronous motors. The authors call for development of technical conditions or state standards with respect to permissible values of voltage, current and rotation rate of sories	
produced asynchronous motors used in frequency controlled electrical drive systems. An example of the calculation is presented. Orig. art. has: 19 formulas.	- C
SUB CODE: 09 / SUBM DATE: 17May65 / ORIG REF: 006	
Cord 1/1 gd UDC: 62-83-531.6	





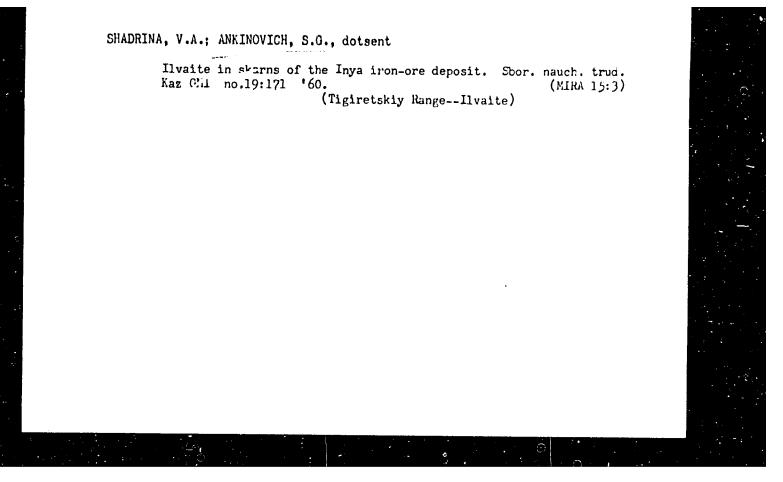


AMKINOVICH, Ye.A., kand.geologo-mineralogicheskikh nauk; ANKINOVICH, S.G., kand.geologo-mineralogicheskikh nauk

Composition of the vanadium-bearing horizon in the Kara-Tau.

Sbor.nauch.trud.KazGMI no.18:49-68 '59. (MIRA 15:2)

(TAYE-Tau--Vanadium)



ANKINOVICH, Stepan Gerasimovich; SHIYGIN, Ye.D., prof., doktor geologomineralog. nauk, otv. red.; RZHONDKOVSKAYA, L.S., red.; ALFERO-VA, P.F., tekhn. red.

[Lower Peleozcic of the vanadium-bearing basin in the northern Tien-Shan and the western margin of central Kazakhstan] Nizhnii paleozoi Vanadienosnogo basseina Severnogo Tian'-Shania i zapadnoi okrainy TSentral'nogo Kazakhstana. Alma-Ata, Izd-vo Akad. nauk Kazakhskoi SSR. Pt.1. 1961. 270 p. (MIRA 14:9)

1. Institut geologicheskikh nauk AN Kazakhskoy SSR (for Ankinovich). (Kazakhstan—Vanadium) (Tien Shan—Vanadium)

BOX, Ivan Ivanovich; BORUKAYEV, R.A., akademik, glav. red.;

ANKINOVICH, S.G., doktor geol.-miner. nauk, otv. red.;

NESTEROVA, I.I., red.; KOVALEVA, I.F., red.

[Oros of agricultural importance; fundamentals of their geology and their prospecting and evaluation indicators] Agronomicheskie rudy; osnovy ikh geologii i poiskovo-otsenochnye priznaki. Alma-Ata, Nauka, 1965. 305 p. (MIRA 18:9)

1. Akademiya nauk Kaz.SSH (for Borukayev).

ANKINOVICH, YE. A.

"New Mineral Kurumsakite," Izv. AN KazakhSSR, No 134, ser. geol., No 18, 116-117, 1954

In the horizon of the bituminous shales in northwest Karatau has been observed a mineral which is encountered exclusively in the oxidation zone and, as a rule, is said to be not less than 10 meters from the surface. The mineral, named kurumsakite, after the place of its location, is encountered in the walls of cavities and crevices in the form of greenish-yellow and bright-yellow fine crystalline powders of a divergent (radial) and felted structure; partially it forms very fine plates in the shape of elongated hexagons.

RZhGeol, No 1, 1955

15-57-7-9402

Referativnyy zhurnal, Geologiya, 1957, Nr 7, Translation from:

pp 95-96 (USSR)

AUTHOR:

Ankinovich, Ye. A.

TITLE:

Shteygerit (?) in the Bituminous Shales of the Northwestern Kara-Tau (Shteygerit v bituminoznykh slantsakh Severo-Zapadnogo karatau)

PERIODICAL:

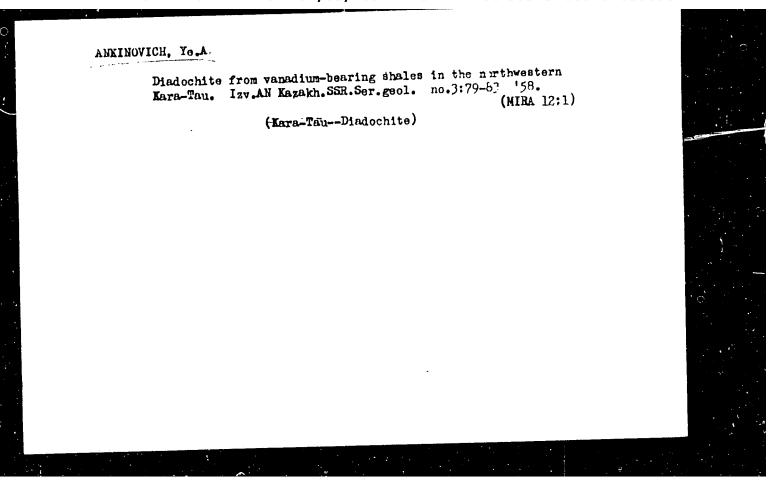
Sb. nauch. tr. Kazakhsk. gorno-metallurg. in-t, 1956,

Nr 13, pp 77-79

ABSTRACT:

Shteygerit has been identified in association with a group of colloidal minerals in the oxidized zone of one of the Cambrian horizons, in places where alteration has been most intense. The microscope shows the mineral to consist of an aggregate of matted, fibrous, very fine crystals of a clear yellowishgreen color. The size of separate individuals does

Card 1/2

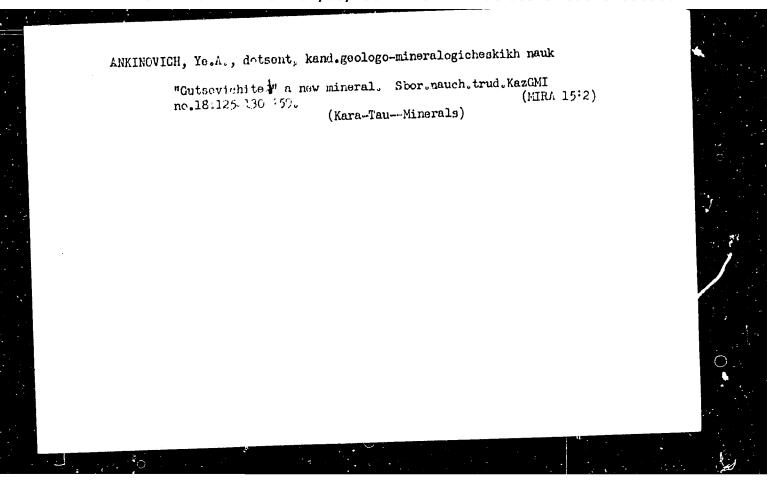


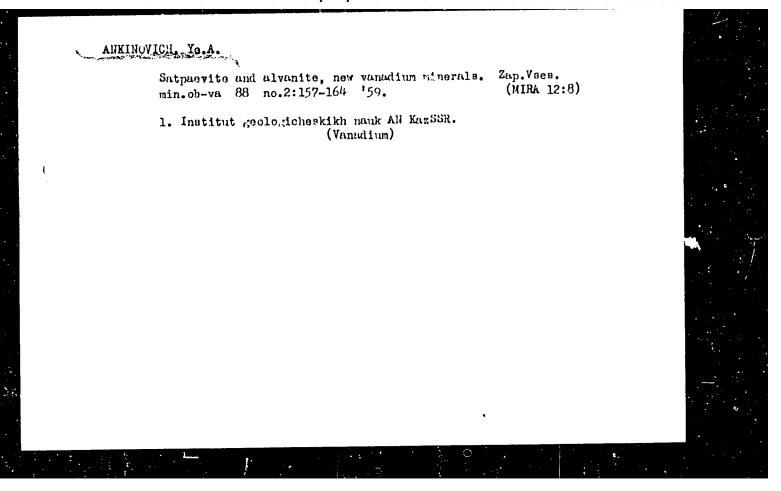
ANKINOVICH, Ye.A., kand.geologo-mineralogicheskikh nauk; ANKINOVICH, S.G., kand.geologo-mineralogicheskikh nauk

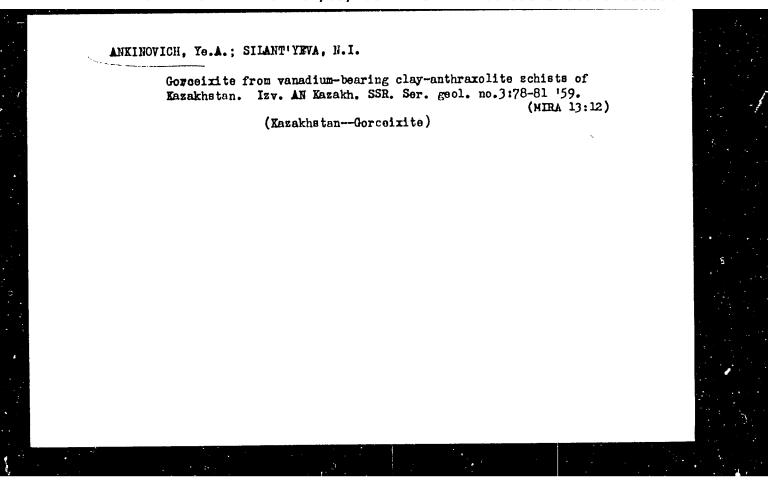
Composition of the vanadium-boaring horizon in the Kara-Tau.

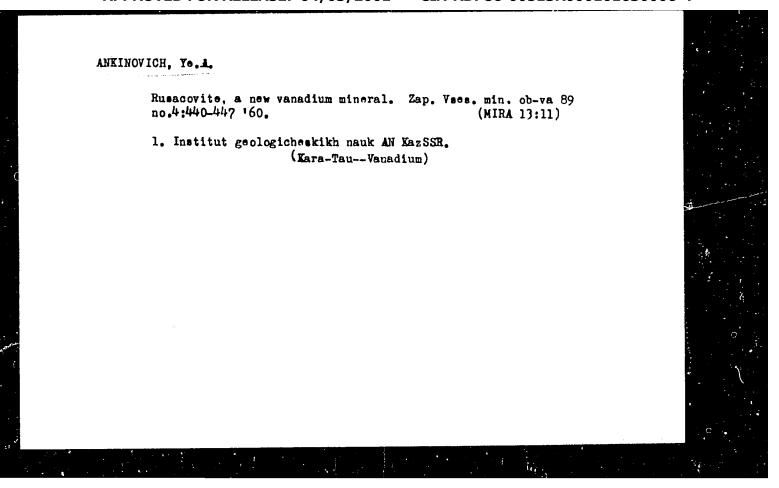
Sbor.nauch.trud.KazGMI no.18:49-68 159. (MIRA 15:2)

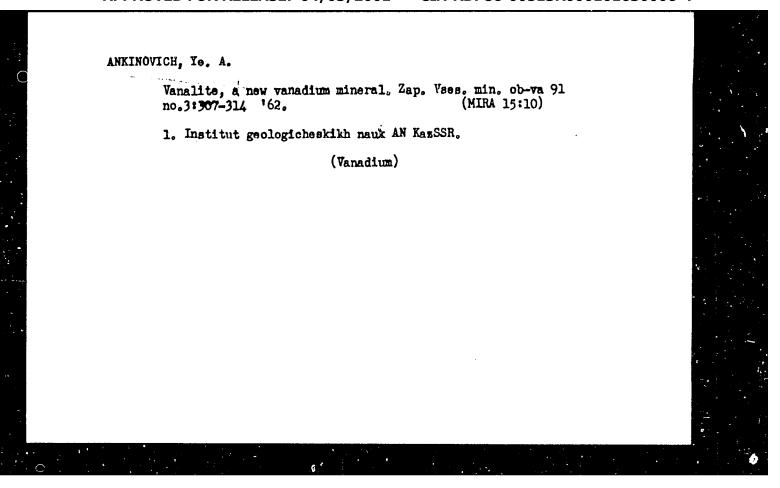
(TAra-Tau-Vanadium)

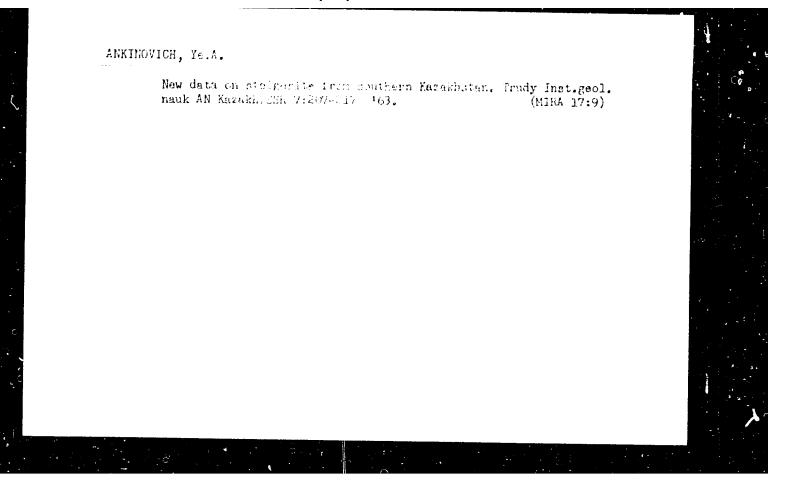


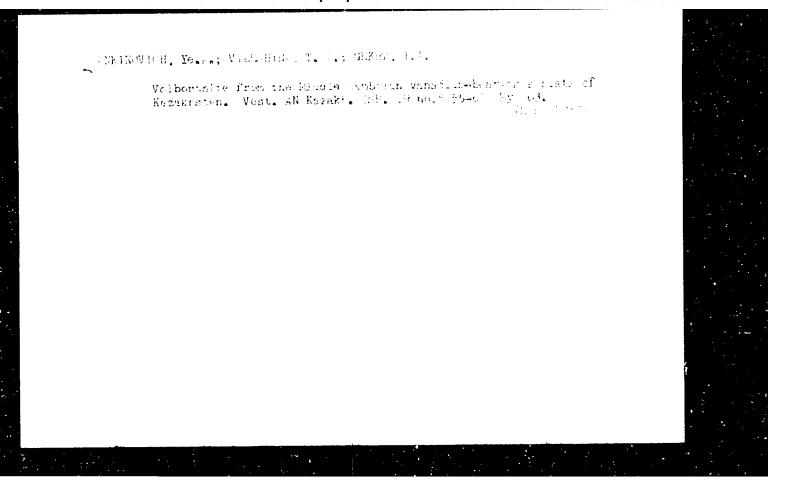


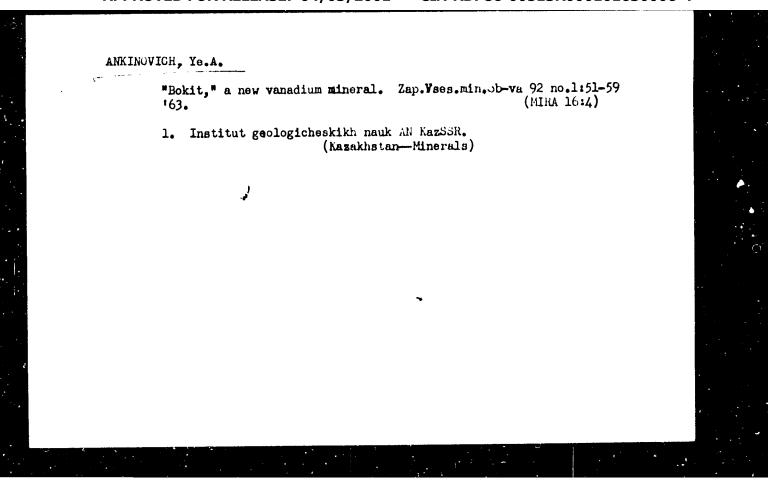








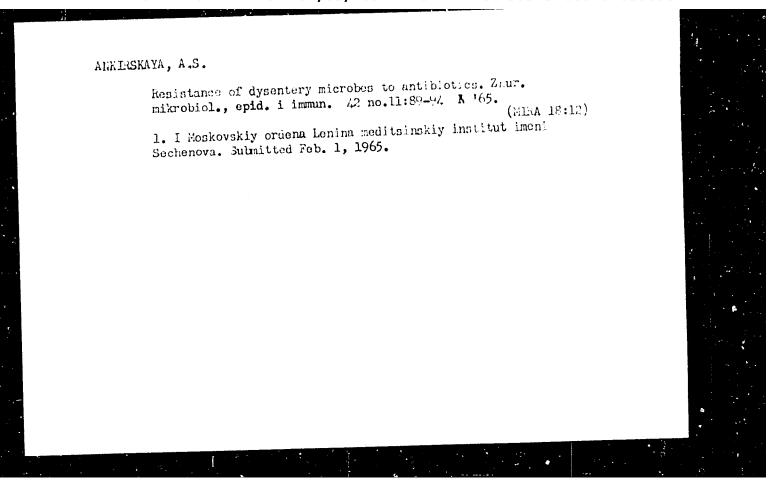




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Carborate cyanotrichite, a new variety of cyanotrichite. Zap.Vses.min.
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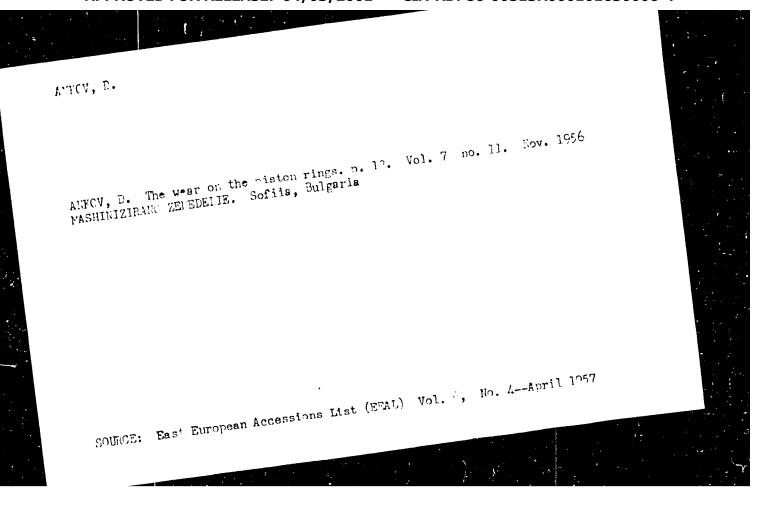


"Device for removing the axle of the idler gear wheel of the 1-MA (for ACKHT-NATI) and the D-54 (for DT-54) motors."

1. 26 (Ratsionalizatsiia) Vol. 7, no. 6, June 1957

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AUTHORS Arbecime V. N. Zluto erkic nike L. F

T!TLE-Calculation of the Over all Stability of Hydrotechnical Structures According to the Limiting state Method (Raschet Ashchev uster n. Asti gidrotekuni, heskikh scoruzhen y po mercdu predel rykh

SOUTH Aries

PER'OD'CAL Tr. Trent: policin tamerski flota 1957. Nr. (2. pp. 40. 4).

ABSTRACT The method of circular cylindrical slip surfaces is used to substantiate the calculation of the over all stability of hydroto the call structure foundations. The essence of this method con state in the reducing a stab lifty compleient as the criterion of the coer all stab (its. This stab. Lits coefficient is obtained from the querient or the moments of the forces resisting the apporting of the structure and the upsetting forces both relative to the center of the arc or slip passing this or the four dation. A compart son ) - made c, this method and the method of calculating the c erigin

stablity of journations according to the limiting state proposed. Card 1/2 by D Ye Po sho and R A Tokar Priblizherney

Calculation of the Over all State I ty of Hydrotechnical Structures (com.)

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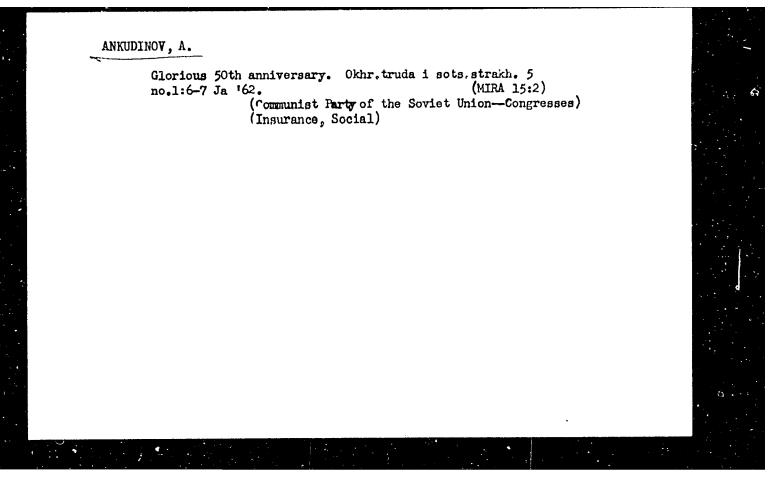
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	1. Novocherkasskiy politekhnicheskiy institut, kafedra analiticheskoy khimii.	
	(MolybdenumAnalysis)	о о
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Effect of the verticity of external flow and of the curvature of a body on the flow in a boundary layer. Inah. zhur. 2 no.4:262-268 '62. (MIRA 16:1)

(Boundary layer)

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IA T	"APPROVED FOR RELEASE: 04/03/2001  DATE: 66 ENT(d)/ENT(1)/ENP(e)/FUN/ENT(N)/ENT(N)/ENT(N)/ENT(N)/ENT(N)/ENT(N)/ENT(N)/ENT(N)/ENA(1)  DESSION NR: AP5025121 ENP(N)/ENA(1)  WITHOR: Ankura Vy	(w)/IP (c)/ENT(1)/ENT(v)/EDT(1)/200/0966  (p(b)/ UR/02)8/5/25/00 25/00 2900/0966  Sayer on blunted cones in supersonic  matematicheskoy fiziki, v. 5, no. 5,  matematicheskoy fiziki, v. 5, no. 5,  ow, boundary layer, stagnation point,  ow, boundary layer, stagnation point,  number, friction coefficient  number, friction coefficient  number, friction and procedure  c gas flows are presented in the case of  c gas flows are presented in the case of  insulated wall. An analytical procedure  insulated wall equations describing an axisym-  ferential equations describing of the  ferential equations describing of the
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